High-throughput measurement of the influence of pH on hydrogen production from BaTiO$_3$/TiO$_2$ core/shell photocatalysts

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Abstract

The rates of hydrogen production from four different BaTiO$_3$/TiO$_2$ core/shell photocatalysts and their components were measured as a function of pH using a parallelized and automated photochemical reactor (PAPCR) to determine the optimized structure and pH condition for photochemical hydrogen production. The amount of hydrogen produced by each reactor in a 96-reactor array was quantified by the color change of a hydrogen-sensitive material. For the core/shell photocatalysts annealed at 600 °C, the increase in hydrogen production rate with pH at pH 3-9 is ascribed to the adsorption of more negatively charged species that bend the bands upward, promoting hole transport to the surface and the oxidation half reaction. At intermediate pH, the core/shell catalyst annealed at 600 °C had the highest reactivity, indicating that the generation and transport of charge carriers were improved by the BaTiO$_3$/TiO$_2$ core/shell structure. The results demonstrate that PAPCR is an effective way to compare the performance of hydrogen-producing catalysts with different structures and in different operating conditions.

Keywords

Photocatalytic hydrogen generation; pH effect; High-throughput measurement; BaTiO$_3$/TiO$_2$ core/shell photocatalysts; Surface charge.
1. Introduction

Currently available photocatalysts do not split water efficiently enough to be commercially competitive for hydrogen production[1]. A variety of modifications have been applied to photocatalysts to accelerate photochemical reactions[2–17]. Most of these modifications have been focused on engineering the catalysts themselves by doping[9–12] or by modifying the surface[8,13–15]. The efficiency of photochemical reactions can also be manipulated by changing the species in aqueous solution. For example, it is simple to tune the pH of the solution, which is effective as long as the catalyst is stable over the pH range[4–7,16,17]. A variation in the adsorption of solution species at the catalyst-solution interface leads to a change in the surface charge and, with it, the shapes of the bands within the catalyst. The shapes of the bands influence the transport of charge carriers to the interface, promoting or suppressing the reaction. The effect of pH on the photochemical reactivity has been studied for relatively simple materials systems, including TiO$_2$[16,17], BaTiO$_3$[4,5], and ZnO[6,7]. However, to the best of our knowledge, the effect of pH on the reactivity of a core/shell catalyst, especially one that has proven to be more efficient than the constituent materials, has not been extensively studied. Computational investigations of TiO$_2$ coated BaTiO$_3$ indicated that a maximum in reactivity should occur at pH values slightly higher than neutral pH, where the two electrochemical half reactions were balanced[18]. Understanding the effect of pH on a core/shell catalyst will make it possible to control both the catalyst's structure and the solution conditions to improve reactivity.

The spontaneous polarization of ferroelectric BaTiO$_3$ has been used to improve the transport of charge carriers and thus to accelerate photochemical reactions[19,20]. In
addition to promoting the transport of charge carriers to the surface, the separation to 
spatially distinct domains increases the carrier lifetime[21]. Note that BaTiO$_3$ has a 
bandgap of 3.2 eV[22], so it is a UV light absorbing material. BaTiO$_3$ has been coated 
with TiO$_2$ to prevent decomposition[23] and increase the surface area in contact with 
solution[24]. A previous study of a TiO$_2$ coated BaTiO$_3$ photocatalyst at a fixed pH 
showed that maximum reactivity required a synthesis temperature high enough to 
promote crystallinity and bonding at the BaTiO$_3$/TiO$_2$ interface, but not so high that the 
surface area was compromised. Particulate catalysts were also fabricated from similar 
took advantage of the light absorption and ferroelectric polarization of the PbTiO$_3$ core, 
and the large surface area of the TiO$_2$ shell[25]. A CdTe/CdS core/shell catalyst combined 
the extended absorbance region of the core and the chemical stability of the shell[26]. In 
another catalyst, the charged surface domains of a BiPO$_4$ core or the band potential 
difference between the C$_3$N$_4$ shell and the BiPO$_4$ core promoted the separation and 
transport of electron-hole pairs at the core-shell interface[27].

The most common way of evaluating the photochemical reactivity of a catalyst is to split 
water in a gas-tight chamber, extract gas from the reactor headspace at fixed times, and 
measure the amount of hydrogen via gas chromatography. Most photocatalytic advances 
have been confirmed by this method; knowing the amount of photogenerated hydrogen 
and the irradiance of the light source, it is possible to calculate the quantum 
efficiency[28–30]. While this method has been successfully applied to test the 
performance of photocatalysts, it would be difficult to scale this procedure for high 
throughput characterization. The recent development of a colorimetric hydrogen sensitive
material has made it possible to construct a highly parallelized and automated photochemical reactor (PAPCR) for a high throughput measurements of hydrogen production\textsuperscript{[31]}. The PAPCR used here consists of 96 small reactors whose headspaces are covered with a hydrogen sensitive material that darkens in proportion to the amount of hydrogen to which it is exposed. When the relation between the amount of hydrogen in the headspace and the appearance of the hydrogen sensitive material is calibrated, optical images of the hydrogen sensitive material can be used to determine the amount of hydrogen produced throughout the reaction by up to 96 different catalysts in a single experiment.

The purpose of this work is to investigate the effect of pH on the photogeneration of hydrogen by BaTiO$_3$/TiO$_2$ core/shell photocatalysts using a high-throughput method. This BaTiO$_3$/TiO$_2$ core/shell structure combines the high photochemical efficiency of the ferroelectric core with the high surface area and stability of the shell. The results show that, for the core/shell photocatalysts annealed at 600 °C, the reactivity increases with pH in the pH range 3 to 9, decreases at pH 9-11, and reaches its maximum at pH 12. For pH 6, the high-throughput experiment reproduces earlier results obtained by conventional hydrogen production experiments\textsuperscript{[24]}. Furthermore, the BaTiO$_3$/TiO$_2$ core/shell photocatalyst annealed at 600 °C performs better than catalysts annealed at lower and higher temperatures. Taken together, the results show the possibility of accelerating photocatalyst discovery and engineering processes using this high-throughput method.

2. Experimental Methods
The method used to synthesize the BaTiO$_3$/TiO$_2$ core/shell photocatalysts was similar to the process reported previously[32]. Equal weights of micron-sized BaTiO$_3$ (Alfa Aesar) and KCl (Alfa Aesar) were mixed via ball milling with ethanol as the lubricant. The mixture was then stirred for 2 h, before it was dried overnight. The dried mixture was annealed at 1100 °C for 5 h. All annealing processes were carried out in air. Next, the mixture was filtered and washed with boiling deionized (DI) water to remove KCl. The resulting BaTiO$_3$ core particles were dried overnight. Heating the BaTiO$_3$ particles in a molten KCl flux promotes flat surface facets on the particles with relatively fewer defects to support the crystallization of the titania coating. No K or Cl residual was detected in the elemental analysis using energy-dispersive X-ray emission spectroscopy (EDS). Next, the particles were coated with TiO$_2$ using a previously developed procedure that creates a coating with a thickness that optimizes the reactivity[24]. 1 g of the as-synthesized BaTiO$_3$ cores was suspended in a mixture of 9 ml DI water and 20 ml ethanol. The suspension was stirred for 30 min and a few drops of HCl (Fisher Scientific) was added to the suspension to adjust the pH to ≈ 3. Another solution was prepared by mixing 15 ml ethanol, 8.6 ml titanium(IV) n-butoxide (TBOT, Alfa Aesar), and 1 ml of 2,4-pentanedione (Sigma-Aldrich). This solution was then added to the suspension dropwise while the suspension was being stirred. After the final mixture was stirred for 2 h, it was heated under reflux at ≈ 90 °C for 3 h. The product was collected, washed with ethanol, filtered, and dried overnight before it was annealed at a fixed temperature (500, 600, or 700 °C) for 2 h to crystallize the titania. The powders that were annealed at 500, 600, or 700 °C, after adding the TiO$_2$ coating, will be referred to as powder types “5”, “6”, or “7”, respectively. The powder referred to as “nB” is made up of nano-size BaTiO$_3$ cores (100
nm, US Research Nanomaterials, Inc.) coated with titania (using the process described above) and annealed at 500 °C. The powder referred to as "s" consists of the nano-size free-standing TiO$_2$ shell synthesized by the same process and annealed at 500 °C, only without the addition of BaTiO$_3$ cores. The powder referred to as "c" consists of micro-size BaTiO$_3$ cores produced in the KCl flux (uncoated).

To promote hydrogen generation, all of the powders (5, 6, 7, nB, s, and c) were coated with 1 wt.% Pt using an impregnation-reduction method. Powder was added to a H$_2$PtCl$_6$ solution (Sigma-Aldrich) and the suspension was stirred for 2 h. The platinum was then reduced using a five-fold excess of NaBH$_4$ (Acros) and NaOH solution (Acros Organics). After the mixture was also stirred for 2 h, the platinized powders were collected by centrifugation, washed with DI water and dried overnight. Prior characterization of Pt added to the surface using a similar technique has shown that they form islands on the surface 5-10 nm in diameter[33]. Transmission electron microscopy (TEM) images of the BaTiO$_3$/TiO$_2$ core/shell powder were recorded using 2000EX (JEOL) and are presented in Figure S1. The results show the expected structure, similar to the previous reports [24,32].

The suspensions used for hydrogen generation were prepared with the six kinds of powders described above, and a mixture of DI water and methanol. The weights of the powders were measured using an analytical balance (Mettler Toledo). The pH of the DI water was adjusted using NaOH or HNO$_3$ (Fisher Chemical) solutions.

The PAPCR for the high-throughput measurement of photochemical hydrogen generation is illustrated schematically in Figure 1 and described in more detail in reference 28. The as-prepared suspensions were injected into 1.1 ml glass shell vials, which were inserted into an array of 96 holes (8 rows by 12 columns) within a metal holder with an open
bottom, through which light can be transmitted into the reactors. Next, a hydrogen sensitive film (DetecTape, Midsun Specialty Products) was placed on top of the reactor array. The hydrogen sensitive film reacts to an increase in the local hydrogen concentration by changing its color from light to dark. A quantitative relationship between the color change of the film and the local hydrogen concentration was recently established[31]. The calibration details are described in the Supporting Information and the quantitative relationship is shown in Figure S2. The response of the tape to H₂ was calibrated in the concentration range of 0 to 50 % H₂. As illustrated in Fig. S2, the first non-zero point on the calibration curve is at 5 %; when the headspace is 0.7 ml and the total pressure is 1 atm (our most common operating conditions), this corresponds to 2.86 µmol of H₂. We select 5 % as a lower limit for the detection of H₂, although the calibration curve extends to 0 %. To create a gas-impermeable seal in each vial, a film of fluorinated ethylene propylene (FEP) was placed atop the hydrogen sensitive film. To provide a cushion and ensure uniform sealing across all vials, a layer of 1/16” silicone plate was then added, and the whole system was clamped closed with clear plexiglass pressed down with an aluminum flange structure. Four threaded rods pass through the corners of the plate holding the vials, the silicone sealing plate, and the top plate with the window; the entire assembly is then sealed by tightening nuts on the threaded rods to a uniform pressure using a torque wrench.

Light was provided from below by two 100 W UV LED chips (Chanzon), with a peak wavelength of 380 nm. Note that the position of the chips was adjusted so that the light intensity for all 96 vials was approximately the same. The standard error in maximum hydrogen generation rates due to the vials’ different positions relative to the LED chips was 12.3%
measured using 96 identical homogeneous catalyst systems[31]. The UV light source illuminated the reactor array continuously in 6 min intervals. After each 6 min interval, the UV light was turned off, a white light illuminating the hydrogen sensitive film from above was turned on, and a camera recorded an image showing the color of the hydrogen sensitive film that was in contact in the gas in the head space above all 96 reactors. Circulating water was used to cool the LED chips and a fan was used to maintain a constant temperature in the rest of the reactor assembly. The total time of illumination was 6 h, during which 60 images were taken of the hydrogen sensitive film. Eyes should be protected from UV radiation.

The pictures of the hydrogen sensitive film were used to calculate the rate of hydrogen production using the following method. As mentioned above, a relationship between the color of the film and the local hydrogen concentration has been established. In this way, the amount of hydrogen within each vial, at each time interval, can be determined from the contrast in the digital image (up to 50 %). Data from one of the reactors, typical for a catalyst that produces hydrogen, is plotted in Figure 2. Note that there is an incubation time before hydrogen is detected above 5 % (2.86 µmol, indicated by the dashed blue horizontal line). It is assumed the incubation time arises because enough hydrogen has to be produced to saturate the liquid, first, and to surpass the concentration of 5 % in the headspace of the reactor afterwards. The continuous decrease in the slope at longer times is assumed to be caused by the increase in pressure in the headspace as more hydrogen is produced; this will be discussed below. After ignoring points below the calibrated limit and an outlier at ~ 1.7 h (data points colored grey), the rest of the data (plotted with black circles) were fitted to the following logarithmic function:
\[ y = a + b \ln x \]

where \(a\) and \(b\) are fitting parameters. At the intersection of this fitted curve (red solid line) with the lower limit at 5 \% H\(_2\) (blue dashed line), indicated by the green star in Figure 2, the function has its maximum slope, and this slope was assigned to the maximum observable rate of hydrogen production.

The logarithmic fitting was based on the assumption that the reason for the continuous decrease in the rate of hydrogen production was the pressure increase in the headspace with time. The derivation of the logarithmic relationship between the hydrogen production and the reaction time is described in the Supporting Information. Note that previous studies have shown that intermediates including formaldehyde might be the dominant product depending on the reaction time[34]. However, the components of the final product will not influence the logarithmic form of the pressure effect. The justification for modeling the data with the logarithmic function will be discussed further in the following sections.

### 3. Results

To test reproducibility and the effect of pressure, hydrogen production from the catalysts was measured for 6 h, the reactor was opened and left in a well-ventilated hood for several minutes, and a new hydrogen sensitive film was then placed on the same reactors and the reaction was run again under the same conditions. The results of this second reaction are shown in Figure 3. These results are essentially the same as the first reaction (see Figure S3). The circular area above some of the reactors became dark by differing amounts, which is how the film responds to different amounts of hydrogen. The
compositions of the suspensions are tabulated in Table 1. The volume of the suspension was 0.4 ml and all vials contained an aqueous solution with 8 volume percent methanol.

Using images taken every 6 min and the pre-established relationship between the local hydrogen concentration and the color of the thin film, we obtained the hydrogen production versus time for each reactor, as shown in Figure 4. Similar results were found for the first run (see Figure S4). Note that the incubation period and saturation at long times, already discussed with reference to Fig. 2, are common features of almost all reactors that produced a detectable amount of hydrogen. The reproducibility of these reaction characteristics after venting the headspace is consistent with the model that the reaction rate is controlled by the pressure in the headspace. This model is further supported by the fact that the time dependence of the hydrogen generation fits well to a logarithmic function.

Figure 5 shows the maximum observable rates of hydrogen production (normalized by dividing by the weight of the powder in the suspension) for the first six rows of the reactors in the array measured in the second run (see Fig. S5 for data from the first run, which is consistent). The type of the powder and the pH of the solution for the suspensions are labeled. An average rate and the standard deviation calculated from five vials filled with identical suspensions are depicted in the color scale bar. The standard deviation is ≈ 19 % of the average value. The effect of pH on each type of powder is clear by examining each row in Figure 5. It is obvious that there is a maximum rate at pH 12 for all rows and a local maximum at pH 2-3 for most of the rows. Also, it is clear that only the powder annealed at 600 °C is able to maintain measurable hydrogen yields at all pH values, having another local maximum near pH 9. Assuming the mechanism proposed
for the incubation period is correct, then catalysts that produced more hydrogen should have shorter incubation times. The incubation time presented in Figure S6 is consistent with this proposition.

The mass specific rates of hydrogen evolution were previously measured using similar catalysts at pH = 6, but the measurement was carried out by gas chromatography in a conventional reactor system[24]. The comparison between results obtained from these two measurement methods is provided in Figure S7. The current work is consistent with the previous work, which also found that the core/shell catalysts annealed at 600 °C (6) had the maximum rate of hydrogen production and that the next highest rate was from the high surface area titania (s) without a core. However, the absolute values of the mass specific rates of hydrogen production are not the same. Differences in the reactor systems, illumination sources, and methods of measurement, which will be compared in detail in the discussion section, are responsible for the different measured rates. The parameters a and b for both runs are shown in Figure S8 and Figure S9 and the explanations are also provided in the Supporting Information.

Results of powder type “6” and powder type “s” for both the first and the second run were averaged and the data of these two types of powders are compared in Figure 6. Besides the pH effects described above, it is noted that for powder type “6”, there seems to exist a local maximum at pH 9 and a decrease at pH ≈ 10 before it reaches the maximum at pH 12. However, there appears to be no similar local maximum for powder type “s”.

The influence of the weight of catalyst powder on the absolute \(R_{H_2}\) and the mass specific \(R_{m,H_2}\) rate of hydrogen production is illustrated in Figure 7. Similar results were
obtained for the first run (see Figure S10). The volumes of the suspensions (0.4 ml), the pH of the solutions (6), and the methanol volume fractions (8 %) were all the same for these five reactors. The absolute rate of hydrogen production increases with the weight of powder. This is reasonable because more catalyst should generate more hydrogen in a fixed time interval. The mass specific rate of hydrogen production shows an opposite trend. In the ideal case, all mass of the powder would contribute equally and the absolute rate would be a linear function of the weight, while the mass specific rate would be constant. The difference between our result and the ideal case indicates that additional catalyst contributes less to making hydrogen, on a per unit mass basis. A possible reason is that the catalyst in the lowest part of the reactor absorbs most of the light and the catalyst added beyond this point is less active because less light reaches it. It could also result from particle aggregation. The aggregation will become increasingly likely as we add more powder, which limits the contact area between the powder and the solution. Even though the 1.6 mg catalyst loading had the highest mass specific rate, most experiments in this work were carried out using a catalyst loading of 3.2 mg, because this quantity could be weighed and handled with less uncertainty.

Figure 8 shows the effect of the reactor headspace on the mass specific ($R_{m,H_2}$) rate of hydrogen production. This set of experiments was conducted separately from the panel described up to this point. The ratio of the weight of the powder to the volume of the solution (8 mg/ ml), the pH of the solution (12), and the methanol volume fraction (8 %) were all the same for these four reactors. It is noted that a larger headspace means a smaller volume of solution, and since the four suspensions have the same weight of powder to volume of solution ratio, reactors with larger headspaces have a smaller total
amount of catalyst. Interestingly, the absolute reaction rate did not vary significantly with headspace. The mass specific rates were obtained by dividing the absolute rates by weights and are plotted in Figure 8. The increase in the mass specific reaction rate with headspace provides further evidence that increasing pressure in the headspace suppresses hydrogen production because pressure increases more rapidly for smaller headspaces.

The influence of the methanol volume fraction on the mass specific rate of hydrogen production was also investigated. This set of experiments was also conducted separately from the panel described in Table 1. The ratio of the weight of the powder to the volume of the solution (4 mg/ml), the pH of the solution (6), and the headspace (0.7 ml) were all the same for these four reactors. The rate at 8% (2.5×10^3 µmol/h/g) is higher than that at 4% (1.3×10^3 µmol/h/g), but there is no significant change when the methanol volume fraction increases to 12% (2.3×10^3 µmol/h/g).

4. Discussion

It is noteworthy that the mass specific rate of hydrogen production for the core-shell catalyst annealed at 600 °C is greater than that of the other catalysts throughout much of the pH range. The core-shell photocatalyst is thought to be superior to the unsupported catalyst because band bending within the core helps to separate photogenerated charge carriers. Band bending in the core is important because considering the thickness of the anatase TiO_2 shell (50-100 nm), the light absorption coefficients for the BaTiO_3 core (1×10^3 cm^(-1))[35] and the anatase shell (1×10^2 cm^(-1))[36] at the photon energy of 3.27 eV, most photons (>99.9%) would be absorbed by the BaTiO_3 core. Therefore, the majority
of the charge carriers will be generated in the BaTiO$_3$ core and transported to the shell. The pH affects the performance of these catalysts through its effect on surface charge and band bending. Because holes are the minority carriers, it is typically assumed that the oxidation half reaction is rate limiting[37]. Simulations have shown that increasing the negative surface charge (higher pH) increases the upward band bending[18]. While this band bending reduces the rate of the photocathodic reaction, it promotes the photoanodic reaction and thus increases the overall rate of reaction. As the potential increases, the overall reaction rate continues to increase until the photocathodic and the photoanodic reaction rates are equal; at greater potentials the photocathodic reaction becomes limiting and the overall reaction rate decreases. These predicted trends agree with the data in Figure 6 where the hydrogen production rate increases with pH, reaches a maximum at pH 9, and then decreases again to a minimum at pH 11. Note that the unsupported catalyst is not expected to follow this trend because the smaller particles do not support significant band bending[38].

The data at pH 2 and pH 12, where there is a large increase in the amount of hydrogen produced, are not consistent with the changes expected as a consequence of differences in surface charge with pH. Note that the reactivity of the core/shell catalyst is consistent with the shell only catalysts, so the maxima at 2 and 12 are not determined by the core/shell structure, but by something happening with the titania or Pt. The sudden increase in the reactivity at pH 12 may be related to a change in the mechanism of oxidation of the methanol. An important step of methanol oxidation is the formation of formaldehyde from $\cdot$CH$_2$OH. In this step, $\text{H}^+$ is produced and electrons are injected to Pt[34,39]. Therefore, the trapping of electrons on Pt increases when pH increases. The
overall reaction rate is thus improved because the photocathodic reaction rate is increased by the availability of electrons in the Pt. The sudden increase in reactivity at pH 2 might similarly be related to a change in mechanism, but the source of this increase is not currently clear.

The core/shell catalyst annealed at 600 °C had measurable hydrogen yields at all pHs, even at pHs where the other catalysts did not produce hydrogen above the 5 % limit. This suggests that for these intermediate pH values, the structure of the catalyst is the feature that leads to improved reactivity. As noted above, the majority of light is absorbed in the core and must be transported through the shell. Therefore, the BaTiO$_3$ core acts as a photon absorber and supplies carriers to the coating. The ferroelectric domains in BaTiO$_3$ are thought to separate photogenerated charge carriers and reduce recombination[40,41]. Measurements of very long carrier lifetimes in BaTiO$_3$ support this idea[21] and this is the most likely reason for the relatively greater reactivity of the core-shell catalyst at intermediate pH. The superiority of the catalyst annealed at 600 °C compared to those annealed at 500 °C and 700 °C is thought to be related to the structure. As concluded by Li et al.[24], who studied the same catalysts at a single pH near 6, annealing at 600 °C improves the crystallinity of the titania and the quality of the core/shell interface, but annealing above this temperature leads to a dramatic reduction in the surface area and reactivity.

It is interesting to note that the performance of the core/shell catalyst is related to the size of the core. The catalysts labeled "5" and "nB" are both BaTiO$_3$ cores coated with titania and annealed at 500 °C. The one difference is that the catalyst labeled “nB” had 100 nm diameter cores and the catalyst labeled “5” had cores at least ten times larger. The
relatively poorer performance of the catalysts with nanosized cores can be ascribed to difference in the space charge regions in the BaTiO$_3$ core. The width of the space charge region was calculated to be $\approx 100$ nm[42], which is comparable to the particle size of the nano-size BaTiO$_3$, and thus the potential drop within the space charge region was not as great as in the larger cores.

The PAPCR multi-reactor array used in current work produced results that were qualitatively similar to results for the same catalysts measured in conventional gas-tight reactor system[24,32]. However, there were two main differences. The first difference was that the conventional gas-tight reactor system showed neither an initial “incubation” period nor a final saturation regime; the relation between hydrogen yield and time was approximately linear. One reason for this is that the gas-tight reactor was evacuated before irradiation. This was not possible in the PAPCR, so the pre-existing pressure in our reactors suppressed hydrogen generation from the beginning, creating the incubation period. In addition, the conventional reactor had 25 \% more headspace and half the catalyst-to-liquid ratio. Both of these factors contribute to a more rapid pressure increase that suppresses the reaction and leads to the final saturation regime. The second difference between the PAPCR results and the results from the conventional reactor is the difference in the absolute magnitude of the mass specific rate of hydrogen production (which was higher for the PAPCR measurements). This difference is not at all surprising considering that different illumination sources, with different spectral characteristics and illumination geometries, were used. The current work uses light from two 100 W UV LEDs with an emission spectrum narrowly distributed about 380 nm that enters the
reactor only through the bottom of the vial. The conventional reactor used a 57 W medium pressure Hg immersion lamp with emission in the range of 280-388 nm.

The observation of the saturation regime near the end of the experiment is best explained by the pressure build-up in the reactor. One might speculate that this is a result of catalyst degradation or deactivation. However, the fact that the hydrogen yield versus time can be reproduced after venting the reactors shows that the catalyst has not lost activity. From the same observation, one can also see that the loss of activity is not a result of exhaustion of the hole scavenger, methanol. This is supported by the fact that based on the amount of hydrogen produced, only ≈ 1 % of the methanol is consumed by the reaction and that the reaction rate is not strongly sensitive to the methanol concentration. Further evidence for the conclusion that pressure build-up causes the saturation is provided by the observation that the mass specific rate of hydrogen production increases with headspace, as indicated in Figure 8. The additional headspace reduces the rate of pressure build-up. Finally, it is worth noting that the logarithmic behavior that results from the pressure build-up model is consistent with the shape of the hydrogen production versus time data.

It is noted that oxygen remained in the headspace and the solution, which might lead to concerns regarding the back reaction of hydrogen with oxygen on platinum. However, the amount of dissolved oxygen was only ~ 0.1 µmol[43] and the adsorption of oxygen on platinum is negligible without any external bias[44]. Therefore, this back reaction should not be a significant factor that affects the amount of hydrogen detected.

While the response of the PAPCR is not the same as the conventional reactor, the results derived from it are consistent with prior studies of the same catalysts[24]. The significant
advantage of the PAPCR is that up to 96 different catalysts (in the current design) can be tested in the same amount of time as one catalyst in a conventional reactor. This makes it possible to systematically test catalysts prepared in different ways and develop structure-property relationships. For example, the current study showed the effects of core size and annealing temperature on hydrogen production for a BaTiO$_3$/TiO$_2$ core/shell catalyst at a range of pHs. Using the PAPCR to collect large amounts of data may also enable the application of machine learning to identify and engineer more efficient photocatalysts.

5. Conclusions

The effect of pH on hydrogen production from four kinds of BaTiO$_3$/TiO$_2$ core/shell catalysts and their components was measured in a highly parallel experiment. The results from the PAPCR are consistent with results from a conventional reactor at a single pH. The core/shell photocatalysts annealed at 600 °C showed the most interesting pH effect. Within the pH range 3-9, the changes in the rate of hydrogen production with pH were ascribed to the effect of pH on surface potential. At high pH, more negative charge is adsorbed on the surface and this draws more holes (the minority carrier) to the surface to oxidize methanol. The transport of electrons becomes rate limiting when pH is greater than 9, until pH 12, where the injection of electrons into Pt leads to the maximum reactivity. The results show that hydrogen yield from core/shell catalysts is sensitive to both pH and the exact catalyst structure and that these effects can be studied efficiently using a parallel photochemical reactor.

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**Figure 1.** Schematic illustration of the experimental setup for the high-throughput measurement of photochemical hydrogen generation.
Figure 2. Plot of the hydrogen production versus reaction time from one of the reactors. The grey circles are data points that were removed from the set for fitting, while the black circles were used in the fitting. The red curve shows the fitted logarithmic function. The blue dashed line represents a hydrogen concentration of 5%. The green star denotes the position of the intersection of the red curve and the blue line, and the point of maximum slope of the fitted function.

Figure 3. Images of the reactor array, observed from above, (a) before and (b) after the second 6 h run. The diagonal lines are the results of refraction at the interface between the tape and the silicone plate. The two horizontal lines below the 2nd row and the 5th row are the edges of the hydrogen sensitive film. The film was three rows wide and three of them were used to cover the entire reactor array. The brightness, contrast, and the sharpness of the pictures shown above have been adjusted for better presentation, while the hydrogen yield data was extracted from raw images.

Figure 4. The hydrogen production as a function of reaction time for each reactor in the array for the second run. The ranges of the x-axis (0 to 6 h) and the y-axis (0 to 28.6 µmol) are the same for all plots.

Figure 5. Mass specific rate of hydrogen production from suspensions with six types of powders under different pH conditions for the second run. The average value and the standard deviation calculated from five vials containing identical suspensions are depicted in the color scale bar. The bar is twice the standard deviation.

Figure 6. Mass specific rate of hydrogen production from suspensions with powder type “6” (denoted by blue circles) and powder type “s” (denoted by red squares) under different pH conditions. The values and the standard deviation are average values calculated from the first and the second run. The bar is twice the standard deviation.

Figure 7. The effect of the weight of the catalyst on the absolute ($R_{\text{H}_2}$) and the mass specific ($R_{m,\text{H}_2}$) rate of hydrogen production for the second run. The absolute rate is denoted by red squares and the scale on the left axis. The mass specific rate is denoted by blue circles and the scale on the right axis.

Figure 8. The mass specific rate of hydrogen production for different volumes of reactor headspace.
| Powder, pH, (Weight of Powder, mg) | 5, 1 | 5, 2 | 5, 3 | 6, 1 | 6, 2 | 6, 3 | 7, 1 | 7, 2 | 7, 3 | 7c, 1 | 7s, 1 | empty | nB, 2 | nB, 3 | nB, 4 | nB, 5 | nB, 6 | nB, 7 | nB, 8 | nB, 9 | nB, 10 | nB, 11 | nB, 12 |
| 5, 4 | 5, 5 | 5, 6 | 5, 7 | 5, 8 | 5, 9 | 5, 10 | 5, 11 | 5, 12 | 6, 4 | 6, 5 | 6, 6 | 6, 7 | 6, 8 | 6, 9 | 6, 10 | 6, 11 | 6, 12 | 7, 4 | 7, 5 | 7, 6 | 7, 7 | 7, 8 | 7, 9 | 7, 10 | 7, 11 | 7, 12 |
| c, 1 | c, 2 | c, 3 | c, 4 | c, 5 | c, 6 | c, 7 | c, 8 | c, 9 | c, 10 | c, 11 | c, 12 | empty | nB, 2 | nB, 3 | nB, 4 | nB, 5 | nB, 6 | nB, 7 | nB, 8 | nB, 9 | nB, 10 | nB, 11 | nB, 12 |
| 6, 6 | 6, 6, 1.6 | 6, 6 | 6, 6, 6.4 | 6, 6 | 6, 6, 12.8 | 6, 6 | 6, 6, 25.6 | empty | empty | empty | empty | empty | empty | empty | empty | empty |

*For those with only two parameters, the weight of powder, 3.2 mg, was omitted.
Graphical Abstract

Higher Rate of H₂ Production

pH

5 6 7 8 9 10 11 12

Powder

nB c s
Supporting Information for

“High-throughput measurement of the influence of pH on hydrogen production from BaTiO$_3$/TiO$_2$ core/shell photocatalysts”

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Figure S1. TEM images of the BaTiO$_3$/TiO$_2$ core/shell powder (annealed at 600 °C after TiO$_2$ coating).

Hydrogen detection calibration

This new colorimetric chemo-sensitive system was calibrated with known amounts of added hydrogen gas. DetecTape was sealed, with FEP, silicone, and plexiglass, on top of a set of shell vials with holes drilled in the bottom. Custom-made silicone septa, with one side coated in FEP to contain the injected hydrogen, were placed under each vial. Known amounts of atmospheric
pressure hydrogen gas was then inserted through these septa using a gas-tight syringe, and the vials were left to sit for 10 min to allow the tape enough time to provide a reproducible response. Pictures were then taken of the tape and RGB values were extracted for a set of pixels in the center of each well. These values were then averaged and divided by the values from the first image taken prior to the addition of hydrogen. The normalized change in intensity was linear with the $H_2$ concentration and the resulting calibration curve is depicted in Figure S2. This calibration was then used to evaluate the percent hydrogen produced in the parallel photoreactions.

![Calibration Curve](image)

**Figure S2.** Calibration curve for the tape in the photoreactor presented as intensity normalized to intensity without added hydrogen. Percent hydrogen is shown as partial pressure to the total pressure present. Each point is an average of the values taken from various wells placed across the 96 wells.

**The derivation of the logarithmic relationship**

According to the theory of pressure effects on reaction rates,$^1$

\[
\ln k = \ln k_0 - \frac{\Delta^+ V^0}{RT} P
\]
where \( k \) is the rate constant at pressure \( P \); \( k_0 \) is the rate constant at zero pressure; \( \Delta \nabla V^0 \) is the volume change in going from the initial state to the activated state, known as the volume of activation; \( R \) is the universal gas constant; and \( T \) is the temperature. It was assumed that the temperature was constant and the volume of activation was independent of pressure. The overall photochemical reaction in this work was assumed to be:\(^2\)

\[
CH_3OH + H_2O \rightarrow 3H_2 + CO_2
\]

The rate of this reaction can be defined as:

\[
r = \frac{1}{3} \frac{dp_{H_2}}{dt} \tag{2}
\]

where \( p_{H_2} \) is the partial pressure of hydrogen. Note that the rate of the reaction can be linked to the rate constant as follows:

\[
r = k[CH_3OH]^n[H_2O]^m \tag{3}
\]

where \( n \) and \( m \) are the reaction orders, and \([CH_3OH]\) and \([H_2O]\) are the concentrations of methanol and water, respectively. Based on the highest calibrated limit for the amount of hydrogen (28.6 \( \mu \)mol), the consumption of methanol and water in a typical reaction were only \( \sim \) 1 % of the initial volume. Therefore, the concentrations of methanol and water were assumed to be constant. Using Equations 2 and 3, we may express the rate constant as:

\[
k = \frac{1}{3} \frac{dp_{H_2}}{dt} \frac{1}{[CH_3OH]^n[H_2O]^m} \tag{4}
\]

The other variable in Equation 1, the pressure \( P \), was estimated to be:

\[
P = P_0 + p_{H_2} \tag{5}
\]

where \( P_0 \) is atmospheric pressure. This expression assumes that the change in pressure was only because of the production of hydrogen. This was based on the fact that the solubility of \( H_2 \) is lower than the minimum calibrated amount.\(^3\) The pressure change due to the generation of \( CO_2 \)
was not included because it is proportional to \( p_{H_2} \); this would only add a constant coefficient to \( p_{H_2} \) in Equation 5. This treatment also shows that the logarithmic form of the pressure effect will not be influenced by the actual components of the final product, including gaseous (\( \text{CO}_2 \)) or non-gaseous (formaldehyde or formic acid) products. Equation 1 can be solved using Equations 4 and 5. The solution takes the form of \( y = a + b \ln x \), where \( y \) is the hydrogen production and \( x \) is the reaction time. The parameters \( a \) and \( b \) are:

\[
a = \frac{V}{\Delta \frac{1}{2} V^0} \ln \left( \frac{\Delta \frac{1}{2} V^0}{RT} e^{ln k_0 \Delta \frac{1}{2} V^0 \frac{1}{RT} P_0 + \ln(3) [CH_3OH]^m [H_2O]^m} \right) \tag{6}
\]

\[
b = \frac{V}{\Delta \frac{1}{2} V^0} \tag{7}
\]

**Figure S3.** The pictures taken above the reactor array at time (a) \( t = 0 \) and (b) \( t = 6 \) h. The diagonal lines are the results of refraction at the interface between the tape and the silicone plate. The two horizontal lines below the 2nd row and the 5th row are the edges of the hydrogen sensitive film. The film was three rows wide and three of them were used to cover the entire reactor array. The brightness, contrast, and the sharpness of the pictures shown above have been adjusted for better presentation, while the hydrogen yield data was extracted from raw images.
**Extra data processing for the first run**

In Figure S4, there is a downward discontinuity at ~ 4 h in the plot for every reactor. This resulted from an abrupt change in the overall brightness of the digital image caused by an instability in the camera or light source. To ameliorate the effect of this artifact, the data from the first 4 h and the last 2 h were processed separately using the method described in the experimental methods section. The separate processing of the different time periods led to two different maximum observable rates of hydrogen production; the larger of the two were defined as the maximum observable rate for this reactor. The data points within the time period having the maximum rate was also used to calculate the incubation time, and parameters $a$ and $b$. This discontinuity was not observed in the second run, and thus the extra processing was not needed.

**Figure S4.** The hydrogen production as a function of reaction time for each reactor in the array. The ranges of the x-axis (0 to 6 h) and the y-axis (0 to 28.6 µmol) are the same for all subplots.
Figure S5. Mass specific rate of hydrogen production of suspensions with six types of powders under different pH conditions shown on a heat map. The average value and the standard deviation calculated from five vials containing identical suspensions are depicted in the color scale bar. The bar is twice the standard deviation.

Figure S6. Color visualization of the incubation time of suspensions with six types of powders under different pH conditions for (a) the first and (b) the second run. The average value and the standard deviation calculated from five vials containing identical suspensions are depicted in the
color scale bar. The error bar is twice the standard deviation. Note that in comparison to Fig. S5, the color scale has been reversed.

**Figure S7.** Comparison between the mass specific rates ($R_{m,H_2}$) of hydrogen production for catalysts synthesized using similar methods yet measured using different methods. The red crosses denote results obtained from PAPCR method (the second run) and the black circles from conventional method (results from ref 4). Note that the results below the 5% limit are plotted as 0 for the PAPCR method.

**Explanations for the parameters $a$ and $b$**

The parameters $a$ and $b$ in $y = a + blnx$ were also obtained for both runs and are presented in Figure S8 and Figure S9. The parameter $a$, which is the y-intercept of $y = a + blnx$, would be zero in the ideal case. However, because of the variable incubation period, during which the minimal detectible amount of hydrogen is formed, it takes non-zero values. As illustrated in Figure S8a and Figure S9a, there is considerable scatter in $a$; the standard deviation in $a$ is $\sim 63\%$ of the average $a$ for both reactions. Because there are no valid data to fit in this time domain, the amount of scatter is not surprising. The parameter $b$ is expected to be a constant. As shown in Figure S8b and Figure S9b, the standard deviation is $\sim 29\%$ of the average value. This range of uncertainty is similar to that of the rate and the incubation time.
Figure S8. Parameters $a$ and $b$ of suspensions with six types of powders under different pH conditions for the first run shown on a heat map. The average value and the standard deviation calculated from five vials containing identical suspensions are depicted in the color scale bar. The error bar is twice the standard deviation.

Figure S9. Parameters $a$ and $b$ of suspensions with six types of powders under different pH conditions for the second run shown on a heat map. The average value and the standard deviation calculated from five vials containing identical suspensions are depicted in the color scale bar. The error bar is twice the standard deviation.
**Figure S10.** The effect of the weight of the catalyst on the absolute ($R_{H_2}$) and the mass specific ($R_{m,H_2}$) rate of hydrogen production. The absolute rate is denoted by red squares and the scale on the left axis. The mass specific rate is denoted by blue circles and the scale on the right axis.

**References**


